<u>Study on bogie strength design</u> <u>considering seismic motion</u>



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Contents

- ✓ Research Background
- Evaluation of the force acting on the bogie frame due to seismic motion
- ✓ Strength evaluation and fatigue damage evaluation for bogie frame

Research Background

When strong forces are applied to bogies due to huge earthquakes, they may suffer damage such as cracks or permanent deformation.

 \Rightarrow From the perspective of running safety, it is important to evaluate the strength and damage of bogie frames exposed to seismic motion.

Example of Shinkansen derailment during an earthquake

(2004.10.23) Joetsu Shinkansen
(2011. 3.11) Tohoku Shinkansen
(2016. 4.14) Kyushu Shinkansen
(2022. 3.16) Tohoku Shinkansen (Stopped)

Niigata Chuetsu Earthquake Great East Japan Earthquake Kumamoto Earthquake Fukushima Earthquake



Joetsu Shinkansen derailment accident



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Evaluate of forces acting on each part of a bogie by analysis of vehicle behavior during an earthquake

Evaluating the forces acting on the bogie frame using multibody dynamics simulation



<u>Analysis of forces acting on each part of a bogie by</u> <u>analysis of vehicle behavior during an earthquake</u>



Load applied to bogie frame



Results of vehicle motion simulation



Results of vehicle motion simulation



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Strength evaluation of bogie frame by FEM analysis



Equivalent stress contour diagram





Extraction of evaluation targets related to the effects of seismic motion

A stress analysis of the bogie frame was conducted assuming a load equivalent to the Northern Pacific Coast Earthquake.



High load areas when seismic motion acts

| | High load area | | | |
|-------------------------------------|--------------------------------------------|----|---------------------------------------|--|
| 1 | Air spring seat | 7 | Joint of side beam/cross beam (Lower) | |
| 2 | Upper surface of cross beam | 8 | Upper surface of side beam | |
| 3 | Edge of Lateral damper seat | 9 | Lower surface of cross beam (Center) | |
| 4 | Joint of connection beam/cross beam(Side) | 10 | Joint of axle beam/side beam | |
| 5 | Joint of connection beam/cross beam(Upper) | 11 | Axle beam seat | |
| 6 | Joint of traction motor seat/cross beam | 12 | Lower surface of side beam | |
| Railway Technical Research Institut | | | | |

Stress time history of the part where the elastic limit was exceeded



Fatigue damage evaluation of bogie frame

fluctuating stress measured in running tests

Running test overview • Measurement object : Bogie frame of Shinkansen trains • Measurement section : Commercial line • Measurement item :

Fluctuating stress

| No | Measurement pint | Max | Min | Stress |
|----|-----------------------------------------------|---------------|---------------|--------------|
| | | Stress MPa | stress MPa | range MPa |
| 1 | Air spring seat | 29 | -20 | 49 |
| 2 | Upper surface of cross beam | 19 | -16 | 35 |
| 3 | Edge of Lateral damper seat | 19 | -23 | 42 |
| 4 | Joint of connection beam/cross beam(Side) | 16 | -7 | 23 |
| 5 | Joint of connection beam/cross beam(Upper) | 24 | -22 | 46 |
| 6 | Joint of support of traction motor/cross beam | 34 | -35 | 69 |
| 7 | Joint of side beam/cross beam (Lower) | 40 | -33 | 73 |
| 8 | Upper surface of side beam | 11 | -9 | 20 |
| 9 | Lower surface of cross beam (Center) | 13 | -10 | 23 |
| 10 | Joint of axle beam/side beam | 23 | -21 | 44 |
| 11 | Axle beam seat | 29 | -18 | 47 |
| 12 | Lower surface of side beam | 27 | -33 | 60 |

Fatigue damage evaluation of bogie frame



Stress frequency distribution in running test

Fatigue damage evaluation for bogie frame

receiving the seismic load



<u>Cumulative damage degree by</u> <u>modified Minor rule</u> $D = \sum \frac{n_i}{N_i}$

Frequency n_i for stress range $\Delta \sigma_i$ Limit fatigue repetition number Ni $D = 1 \Rightarrow$ Fatigue failure

Evaluation of the Effect of Earthquake Motion on Bogie Frames

Cumulative fatigue damage assuming seismic loading

| No. | Evaluation point | Degree of damage due to normal running D _n | Degree of damage due to seismic motion D _{eq} | Total Damage D = D _n + D _{eq} |
|-----|-----------------------------------------------|----------------------------------------------------------------|-----------------------------------------------------------------|------------------------------------------------------|
| 1 | Air spring seat | 0.1340 | 0.0288 | 0.163 |
| 2 | Upper surface of cross beam | 0.0727 | 0.0192 | 0.092 |
| 3 | Edge of Lateral damper seat | 0.0367 | 0.061 | 0.098 |
| 4 | Joint of connection beam/cross beam(Side) | 0.0123 | 0.0093 | 0.022 |
| 5 | Joint of connection beam/cross beam(Upper) | 0.1377 | 0.0337 | 0.171 |
| 6 | Joint of support of traction motor/cross beam | 0.1953 | 0.0274 | 0.223 |
| 7 | Joint of side beam/cross beam (Lower) | 0.2163 | 0.0331 | 0.249 |
| 8 | Upper surface of side beam | 0.0840 | 0.0088 | 0.093 |
| 9 | Lower surface of cross beam (Center) | 0.0680 | 0.0006 | 0.069 |
| 10 | Joint of axle beam/side beam | 0.0913 | 0.0256 | 0.117 |
| 11 | Axle beam seat | 0.1650 | 0.0165 | 0.182 |
| 12 | Lower surface of side beam | 0.2060 | 0.0192 | 0.225 |

 The degree of damage during normal driving is assumed to be 20 million km from the time the car is new to the time it is scrapped.

Evaluation of the Effect of seismic Motion on Bogie Frames



Affect of plastic deformation due to seismic force

| Center of Axle spring seat | Distance between centers of spring mm | Permanent deformation mm | Manufacture tolerance mm | |
|----------------------------------|---------------------------------------------|-----------------------------|-----------------------------|--|
| ①1-2 | 2000 | 0.42 | 0.5 | |
| @3-4 | 2000 | 0.39 | 0.5 | |
| 31-4 | 3202 | 0.15 | 1.0 | |
| ④ 2-3 | 3202 | 0.38 | 1.0 | |

Concept of bogie frame design against seismic motion



<u>...Thank you</u> for your kind attention

